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**A METHOD FOR FITTING LINEARLY SEGMENTED  
MULTI-LAYER ATMOSPHERIC MODELS TO AN ARBITRARY  
SET OF UPPER AND LOWER BOUNDARY CONDITIONS**

R. A. MINZNER



Bedford, Massachusetts

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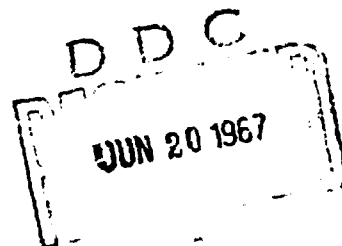
SCIENTIFIC REPORT NO. 4  
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PROJECT NO. 5710

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PREPARED FOR  
AIR FORCE CAMBRIDGE RESEARCH LABORATORIES  
OFFICE OF AEROSPACE RESEARCH  
UNITED STATES AIR FORCE  
BEDFORD, MASSACHUSETTS 01730

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## PREFACE

Atmospheric models are frequently generated for specific regions of the atmosphere in accordance with a particular set of observations. For example, for the region 20 to 90 km or for the region 120 to 100 km altitude. These models are not necessarily extended to sea level, neither are they designed to be continuous with some other existing model at either end of the included range. In some instances it becomes desirable to exactly connect two such models with a transition model atmosphere which for the examples cited would extend between 90 and 120 km. This report discusses a method suitable for generating such transition models.

# ABSTRACT

Any set of temperature, pressure and density values which are realistic for one altitude can be exactly connected to another set of temperature, pressure and density values at a second altitude, with a model atmosphere defined by the appropriate linearly segmented two-layer temperature-altitude profile provided one of these layers is isothermal and the second is a nonzero constant gradient of temperature with respect to height.

The altitude comprising the intersection of the two segments of the required temperature-altitude profile is determined mathematically. The method for generating two-layer models is applied to the generation of three-layer and four-layer models.

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## SECTION I

### REVIEW AND EXTENSION OF THE METHOD FOR DEVELOPING TWO-LAYER TRANSITION MODELS

#### 1. DEFINITION OF THE GENERAL TWO-LAYER TRANSITION MODELS AND THE SPECIFICATION OF THE PARTICULAR CLASS TO BE EXAMINED

Minzner (1966, pp. 5 and 6) has shown that, under a particular though not highly restrictive set of conditions, a two-layer transition model can be made to fit exactly between two sets of fixed boundary conditions. The first consists of a set of realistic values  $H_0$ ,  $\rho_0$  and  $T_0$ , where  $H_0$  is the geopotential corresponding to one arbitrary geometric altitude,  $\rho_0$  is a corresponding realistic value of density, and  $T_0$  is a realistic value of the temperature parameter at  $H_0$ . The second consists of a set of realistic values  $H_n$ ,  $\rho_n$  and  $T_n$ , where  $H_n$  is the geopotential corresponding to another arbitrary geometric altitude,  $\rho_n$  is a corresponding realistic value of density, and  $T_n$  is a corresponding realistic value of the temperature parameter. The subscript immediately to the right of the symbols  $H$ ,  $\rho$ , or  $T$  is associated with the particular geopotential level to which these three quantities are related. In this discussion of transition models, the words altitude or height will be intended to imply the equivalent geopotential without such a statement necessarily being made.

The restrictive conditions defining the particular class of two-layer models to be considered are as follows:

(1) One of the two layers is characterized by a non-zero constant gradient of the temperature parameter relative to the geopotential such that this non-zero-gradient layer extends from  $H_0$  toward  $H_n$  for an unspecified altitude interval to the level  $H_{x_0}$ .

(2) The second layer extending from  $H_{x_0}$  to  $H_n$ , is characterized by a constant zero gradient of the temperature parameter relative to the geopotential. The symbol  $H_{x_0}$  designates the altitude of the interface between the isothermal layer and the non-isothermal layer extending up to  $H_0$ .

The equations and computational procedures for generating the class of transition models as discussed in this report are developed on the basis of two further assumptions: (1) Geopotential  $H_n$  represents a lower altitude level than that represented by  $H_0$  such that the isothermal layer is the lower of the two layers of the transition model, and (2) the value of the temperature decreases with decreasing altitude from  $H_0$  to the isothermal layer. This class of model applies to situations similar to that portion of the U. S. Standard Atmosphere 1962 between altitudes of 117 to 79 kilometers.

The temperature parameter employed in the transition-model development is the molecular scale temperature which combines two variables, the kinetic

temperature and the mean molecular weight of the atmosphere, into a single variable in accordance with the following definition:

The molecular scale temperature, at any level  $H$ , is equal to the ratio of the kinetic temperature to the mean molecular weight, at that same level, times  $M_s$ , the sea-level value of the molecular weight.

For simplicity, the notation commonly used for molecular scale temperature will be avoided in favor of  $T$  in this discussion of transition models, and the word temperature will imply molecular scale temperature.

## 2. DENSITY AND TEMPERATURE RELATIONSHIPS FOR THE SPECIFIED TYPE OF TWO-LAYER MODEL

In the type of model hypothesized, where an isothermal layer at temperature  $T_n$  extends upward from  $H_n$  to  $H_{xo}$  and a layer with a constant non-zero temperature-altitude gradient extends upward from  $H_{xo}$  to  $H_o$ , the density  $\rho_x$  at  $H_x$  may be expressed in terms of  $\rho_n$  and  $T_n$  by the following equations:

$$\rho_{xo} = \rho_n \exp \left\{ \frac{-(H_{xo} - H_n) Q}{T_n} \right\} \quad (1)$$

where

$$Q = \frac{G M_s}{R} = 0.0341631947^\circ K/m' \quad (2)$$

and

- $G$  is the geopotential transformation coefficient equal to  $9.80665 \text{ m}^2 \text{ sec}^{-2} (\text{m}')^{-1}$
- $M_s$  is the sea-level value of the molecular weight of air, 28.9644 kilograms per kilomole (kg/kmol)
- $R$  is the universal gas constant  $8.31432 \times 10^3 \text{ joules } (^\circ K)^{-1} (\text{kmol})^{-1}$

In such a model the density  $\rho_x$  at  $H_x$  may also be expressed relative to  $T_n$  and the upper-level boundary condition values,  $\rho_o$ ,  $T_o$ , and  $H_o$ , which through  $H_x$  imply the value of the non-zero gradient of  $T$  between  $H_x$  and  $H_o$ . Thus,

$$\rho_{xo} = \rho_o \left[ \frac{T_o}{T_n} \right] \left\{ 1 + \frac{(H_o - H_{xo}) Q}{T_o - T_n} \right\} \quad (3)$$

The value of  $H_{xo}$  is found by the simultaneous solution of Equations (1) and (3) as expressed by;

$$\rho_n \exp \frac{-(H_{xo} - H_n) Q}{T_n} = \rho_o \left[ \frac{T_o}{T_n} \right] \left\{ 1 + \frac{(H_o - H_{xo}) Q}{T_o - T_n} \right\} \quad (4)$$

The temperature-altitude gradient between  $H_{xo}$  and  $H_o$  specified by  $L_{xo}$  is given by

$$L_{xo} = \frac{T_o - T_n}{H_o - H_{xo}} \quad (5)$$

Here, the symbol for the gradient has two subscripts, the first designating the unknown lower end of the associated layer and the second designating the known upper end of the associated altitude interval.

### 3. ANALYTICAL EXPRESSION FOR THE GENERATION OF THE TWO-LAYER MODELS

Because it was not at first suspected that an analytical solution for  $H_{xo}$  in Equation (4) could be found, numerical methods involving digital computers were used to determine the value of  $H_{xo}$  for a number of transition atmospheres (Minzner, 1966, pp. 7 to 24). It may now be shown, however, that an analytical solution for  $H_{xo}$  in Equation (4) does exist.

Dividing both sides of Equation (4) by  $\rho_o$  and taking the natural logarithm of both sides of the resulting expression leads to

$$\left[ 1 + \frac{(H_o - H_{xo}) Q}{T_o - T_n} \right] \cdot \ln \left[ \frac{T_o}{T_n} \right] - \frac{(H_n - H_{xo}) Q}{T_n} = \ln \left[ \frac{\rho_n}{\rho_o} \right] \quad (6)$$

The separation of the numerators of the two fractions containing  $H_x$ , so as to permit the extraction of  $H_{xo}$ , followed by a rearrangement of the terms leads to the expression

$$\frac{H_{xo} Q}{T_n} - \frac{H_{xo} Q}{T_o - T_n} \cdot \ln \left[ \frac{T_o}{T_n} \right] = \ln \left[ \frac{\rho_n}{\rho_o} \right] + \frac{H_n Q}{T_n} - \left[ 1 + \frac{H_o Q}{T_o - T_n} \right] \cdot \ln \left[ \frac{T_o}{T_n} \right] \quad (7)$$



Factoring  $H_{x0}$  out of the left-hand side of the equation and dividing both sides of that equation by the remainder of the left-hand side yields

$$H_{x0} = \frac{\ln \left[ \frac{c_n}{c_o} \right] + \frac{H_n Q}{T_n} - \left[ 1 + \frac{H_o Q}{T_o - T_n} \right] \cdot \ln \left[ \frac{T_o}{T_n} \right]}{\frac{Q}{T_n} - \frac{Q}{T_o - T_n} \cdot \ln \left[ \frac{T_o}{T_n} \right]} \quad (8)$$

An evaluation of this expression using the boundary conditions of model Ar (Minzner 1966, Table 2, p. 13) yielded  $H_{x0} = 101.9646$  km. This value agrees, to within one part in the sixth significant figure, with the value obtained by the numerical methods (Minzner, 1966, Table 3, p. 14), and thereby simultaneously substantiates the validity of the numerical method as well as of the analytical solution of  $H_{x0}$  given by Equation (8).

The subscript o to the right of x in  $H_{x0}$  is used to indicate that this particular value of  $H_x$  is calculated with the upper boundary conditions at level  $H_o$ . If, as will be seen in the generation of a three-layer model,  $H_x$  is calculated from some other upper-level boundary condition, as at  $H_m$ , the notation associated with x will be m as in  $H_{xm}$ .

The value  $H_{x0}$  from Equation (8), and the value  $L_{x0}$  from Equation (5), along with the upper and lower set of boundary conditions completely define the only two-layer transition model, of the type under consideration which satisfies the boundary conditions. There are multilayer models (three or more layers), however, which satisfy the same upper and lower set of boundary conditions and the unique two-layer model serves as a basis for the generation of these multilayer models. Computer Programs for the generation of two-layer models are given in Appendix A.

## SECTION II

### GENERATION OF THREE-LAYER MODELS

The method for the generation of a two-layer model between upper and lower boundary conditions can be extended to the generation of an infinite number of three-layer models. The method consists essentially of arbitrarily selecting an altitude interval for the uppermost layer, computing the conditions at the base of that layer from the initial upper-boundary conditions, and using these new values as the basis for the computation of the related two-layer model. The detailed steps to be used are as follows:

(1) Compute the value of  $H_{x0}$  and  $L_{x0}$  for that two-layer model which fits the initial boundary conditions.

(2) Select a suitable value  $H_1$  as the base of the uppermost or first layer of the desired three-layer model. A suitable value meets the condition  $H_{x0} < H_1 < H_0$ . An infinite number of possible values of  $H_1$  exist between  $H_{x0}$  and  $H_0$ .

(3) Select a suitable value of  $L_1$  for the layer  $H_0$  to  $H_1$ . It may be demonstrated that if the gradients of the several layers are to decrease monotonically from  $H_0$  to  $H_n$ , the value of  $L_1$  must meet the condition  $L_{x0} < L_1$ .

Furthermore, it will be seen that  $L_1$  must meet the condition  $L_1 < L_{max}$  where  $L_{max}$  is an upper limit associated with  $T_{1min}$  at  $H_1$  as in Figure 1. The determination as to whether  $L_1 < L_{max}$  is based upon the result of a test following a later step in the procedure. At this point, however, a trial value of  $L_1$  is chosen. An infinite number of possible values of  $L_1$  meet the necessary condition  $L_{x0} < L_1 < L_{max}$ .

(4) Compute  $T_1$  at the selected value  $H_1$  from the selected value  $L_1$  using the relationship

$$T_1 = T_0 - L_1 (H_0 - H_1) \quad (9)$$

(5) Compute the value of  $\rho_1$ , the density at  $H_1$ , using the relationship

$$\rho_1 = \rho_0 \left[ \frac{T_0}{T_1} \right] \left\{ 1 + \frac{(H_0 - H_1) Q}{T_0 - T_1} \right\} \quad (10)$$

The set of values  $H_1$ ,  $T_1$ , and  $L_1$  serve as a new upper-boundary condition which with  $H_n$ ,  $T_n$ , and  $P_n$  provide the means for generating a two-layer model between  $H_1$  and  $H_n$ , where these two layers are designated layers 2 and 3 of the three-layer model. The interface between layers 2 and 3 is designated  $H_{x1}$ .

(6) Determine  $H_{x1}$  using Equation (8) with suitable subscript modifications, i.e., subscript zero is changed to one. If  $L_1$  has been properly selected in step 3,  $H_{x1}$  will be found to have a value such that  $H_n < H_{x1} < H_{x0}$ , and this condition serves as the test for suitability of  $L_1$ .

(7) Compute the gradient for the layer between  $H_{x1}$  and  $H_1$  by using Equation (5) with the subscript zero increased to subscript 1.

The conditions for the test of suitability of  $L_1$  based on the value of  $H_{x1}$  have been developed through the following argument:

It is apparent that if  $L_1$  is selected to be equal to  $L_{x0}$ ,  $H_1$  is not really the base of a new layer, but is a level within the layer  $H_{x0}$  to  $H_0$ . Computations based on  $H_1$ ,  $T_1$ , and  $L_1$  would then yield  $H_{x1} = H_{x0}$ , and one would have determined only a redundant case of the original two-layer model. As the value of  $L_1$  is allowed to increase from  $L_{x0}$ , for a fixed value of  $H_1$ , the value of  $H_{x1}$  progressively decreases from  $H_{x0}$  until, in the limit for  $L_1 = L_{max}$ , the value of  $H_{x1}$  becomes identically  $H_n$  in which case the isothermal layer has vanished as indicated in Figure 1. For values of  $L_1 > L_{max}$ , the computed values of  $H_{x1}$  become less than  $H_n$ , indicating an impossible situation.

It is also possible to select values of  $L_1$  such that  $L_{min} < L_1 < L_{x0}$ . As  $L_1$  is decreased from  $L_{x0}$ , the value of  $H_{x1}$  increases from  $H_{x0}$  until for  $L_{min}$ ,  $H_{x1} = H_1$ . For this case, layer 2 has the impossible conditions of zero thickness and an infinite temperature gradient. All values of  $L_1 < L_{x0}$  are impossible however, if the model is constrained to one having a monotonically decreasing set of values of  $L$  for successive layers. It follows therefore, that the only suitable values of  $L_1$  are those which lead to values of  $H_{x1}$  such that  $H_n < H_{x1} < H_{x0}$ . An infinite number of such values exist.

If values of  $L_1$  are constrained to be integral multiples of some fixed values  $\Delta L_1$ , and if they are constrained to be within the range  $L_{x0}$  to  $L_{max}$ , the smallest suitable values of  $L_1$  may be expressed as

$$L_{1a} = j_1 \Delta L_1 \quad (11)$$

where  $j_1$  satisfies the inequality

$$\frac{L_{x0}}{\Delta L_1} < j_1 \leq 1 + \frac{L_{x0}}{\Delta L_1} \quad (12)$$

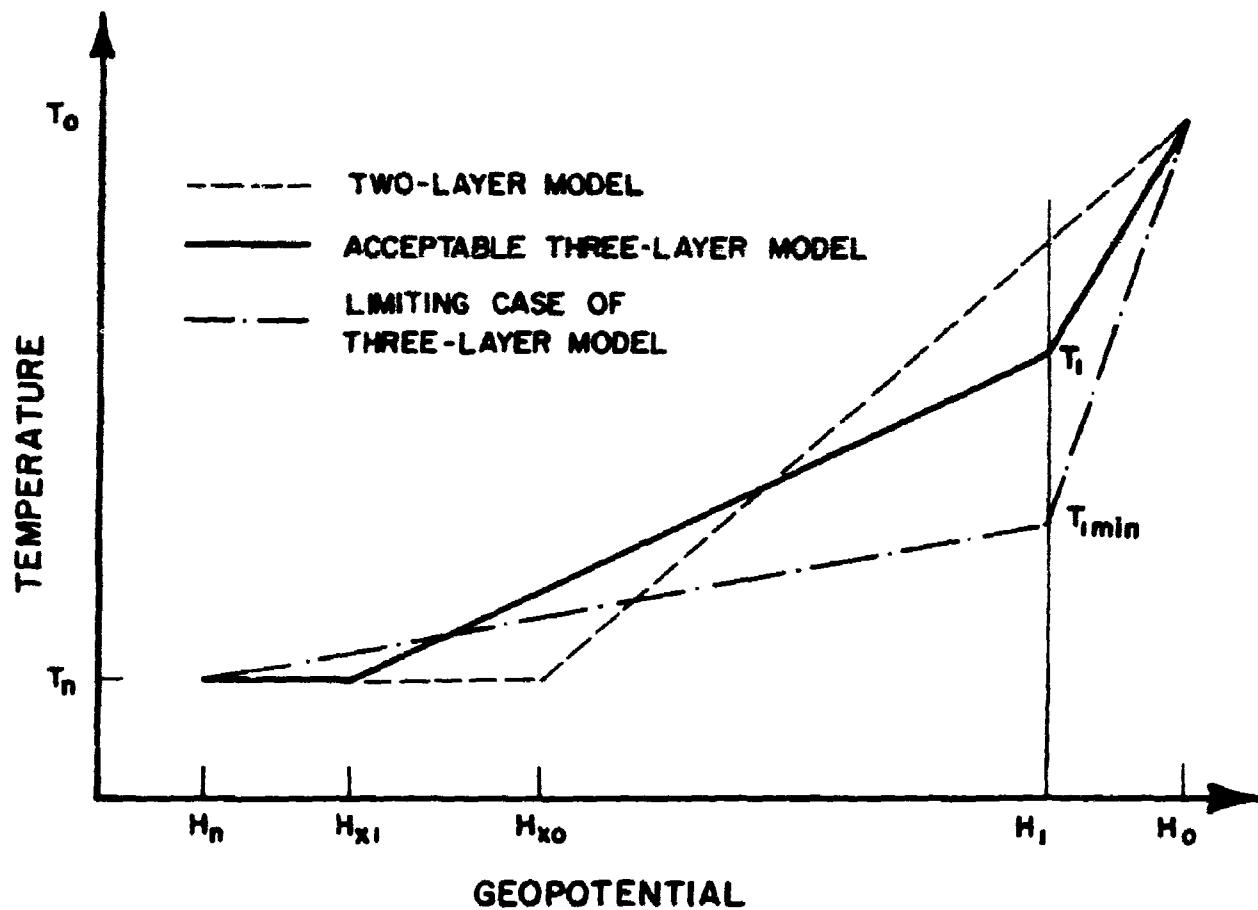


Figure 1. Schematic temperature-altitude diagram for a two-layer model atmosphere, for an acceptable related three-layer model, and for a limiting case of the three-layer models.

The series of acceptable values of  $L_1$  and the related series of values of  $H_{x1}$  are then

$$L_{1a} = (j_1 + 1 - 1) \Delta L_1, \quad H_{x1a} \quad (13a)$$

$$L_{1b} = (j_1 + 2 - 1) \Delta L_1, \quad H_{x1b} \quad (13b)$$

$$L_{1c} = (j_1 + 3 - 1) \Delta L_1, \quad H_{x1c} \quad (13c)$$

etc., until a value  $L_{1\delta}$  is reached for which  $H_{x1\delta}$  is less than  $H_n$ . This situation is shown schematically in Figure 2.

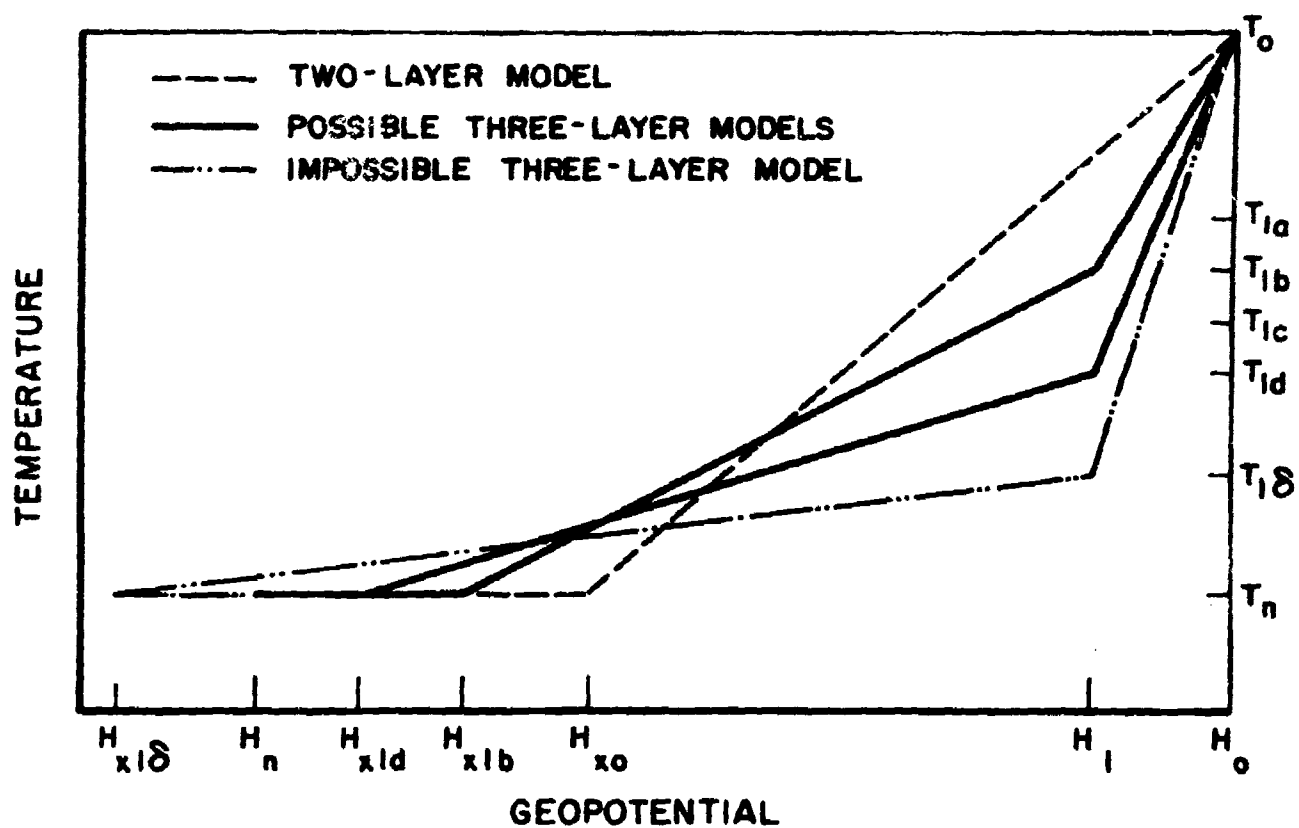


Figure 2. A schematic temperature-altitude diagram showing four possible three-layer models and one impossible three-layer model.

### SECTION III

#### GENERATION OF MULTILAYER MODELS

The above procedure may be extended to the generation of four-layer models and on to the generation of n-layer models. The procedure consists of generating a three-layer model as indicated above, and then taking the lower two layers of this model, follow the procedure of steps 2 through 7 of Section II, but with subscript 1 replaced by subscript 2, and subscript 0 replaced by subscript 1. In a similar manner, the procedure may be extended to a model of any number of layers.

The altitudes specifying the boundaries of the four layers of each of a set of several possible four-layer models for a specified set of boundary conditions are given in Table 1.

TABLE 1

DEFINITIONS OF POSSIBLE FOUR-LAYER MODELS  
CONSISTENT WITH THE BOUNDARY CONDITIONS  
RHOC = .246100E-07 KG/M3, TC = 382.244 DEG K AT HC = 117776.0 M  
RHON = .198200E-04 KG/M3, TN = 190.650 DEG K AT HN = 79000.0 M  
AND WITH THE ASSIGNED VALUES OF H AND DL,  
H1 = 110000.0 DL = .100000E-02  
H2 = 105000.0 DL = .100000E-02

MINIMUM HEIGHT FOR BASE OF LAYER 1 IS HX0 = 100503.0 M.  
MINIMUM GRADIENT FOR LAYER 1 IS GLX0 = .110921E-01 DEG/M.

SET-01 MODELS DEFINED BY LAYER-1 GRADIENT OF 12 DEG/KM.

MINIMUM HEIGHT FOR BASE OF LAYER 2 IS HX1 = 99731.2 M.  
MINIMUM GRADIENT FOR LAYER 2 IS GLX1 = .957098E-02 DEG/M.

MODEL 1 OF SET 01 DEFINED BY LAYER-2 AND -1 GRADIENTS, 10 AND 12 DEG/KM.

LEVEL	H METERS	RHO KG/M3	T DEG K	L DEG/M
0	117776.0	.246100E-07	382.244	
1	110000.0	.722249E-07	288.932	.120000E-01
2	105000.0	.167158E-06	238.932	.100000E-01
3	99731.2	.513486E-06	190.650	.860190E-02
4	79000.0	.198200E-04	190.650	.000000E+00

MODEL 2 OF SET 01 DEFINED BY LAYER-2 AND -1 GRADIENTS, 11 AND 12 DEG/KM.

LEVEL	H METERS	RHO KG/M3	T DEG K	L DEG/M
0	117776.0	.246100E-07	382.244	
1	110000.0	.722249E-07	288.932	.120000E-01
2	105000.0	.171873E-06	233.932	.110000E-01
3	98452.7	.607072E-06	190.650	.661069E-02
4	79000.0	.198200E-04	190.650	.000000E+00

MODEL 3 OF SET 01 DEFINED BY LAYER-2 AND -1 GRADIENTS, 12 AND 12 DEG/KM.

LEVEL	H METERS	RHO KG/M3	T DEG K	L DEG/M
0	117776.0	.246100E-07	382.244	
1	110000.0	.722249E-07	288.932	.120000E-01
2	105000.0	.176835E-06	228.932	.120000E-01
3	97275.3	.749666E-06	190.650	.495581E-02
4	79000.0	.198200E-04	190.650	.000000E+00



#### REFERENCES

Minzner, R. A., 1966: "Studies of Atmospheric Structure and Variability of the Earth's Atmosphere," GCA Technical Report No. 66-14-N, Final Report, Contract No. NASW-1225.

## APPENDIX A

### Program 1

The program for defining a two-layer transition model atmosphere by the method of successive approximation and from the definition computing the various properties as indicated in Tables 3 through 10 of the final report on Contract No. NASW-1225 (Minzner, 1966).

# PROGRAM 1

```

C SOURCE DECK FOR THE COMPUTATION OF TWO-LAYER TRANSITION MODEL
C ATMOSPHERES BETWEEN UPPER LAYER AND LOWER LAYER BOUNDARY CONDITIONS
C WHEN THE FOLLOWING CONDITIONS REGARDING TEMPERATURE-ALTITUDE
C GRADIENT PREVAIL:
C 1. IT HAS A DIFFERENT CONSTANT VALUE FOR EACH LAYER,
C 2. IT HAS A POSITIVE VALUE FOR THE UPPERMOST LAYER,
C 3. IT HAS A ZERO VALUE FOR THE LOWEST LAYER,
C THE METHOD INVOLVES THE SIMULTANEOUS NUMERICAL SOLUTION OF
C TWO EQUATIONS USING THE METHOD OF SUCCESSIVE APPROXIMATIONS
C AS DISCUSSED BY MINZNER IN GCA TECH RPT. NO.66-14-N
C JUNE 1965, REVISED MARCH 1966
12 READ 101,DEG,HR,HPR,PHR,HA,HPA,PHA,FMON,T1,T2
      READ IN INITIAL CONDITIONS FOR MODEL
      T1 AND T2 ARE THE TITLE FOR THE MODEL
131 FORMAT(A3,F4.0,F10.7,F11.4,F9.4,F9.5,F10.3,1XA4,2A5)
      READ 115,FL,HBR
116 FORMAT(F4.1,1XF5.0)
      F=2.71828183
      EPSI=.1E-08
      X=HR+.1
      PUNCH 112
112 FORMAT(35HPROPERTIES OF TRANSITION ATMOSPHERE)
      PUNCH 106,T1,T2,DEG,FMON
106 FORMAT(2A5,2X1H(,A3.1H),2XA4,4X17HTO JACCHIA MODELS/)
C SOLVE THE TWO EQUATIONS SIMULTANEOUSLY USING
C THE METHOD OF SUCCESSIVE APPROXIMATIONS
      2 BETA=(HA-X)/(HPA-HPR)
      Y=(1.+BETA)*LOG(HPA/HPR)+LOG(PHA)
      XOLD=X
      X=-{Y-LOG(PHR)}+HPR/LOG(E)+HB
      IF(SENSE SWITCH 1) 4,3
C SENSE SWITCH 1 ON WILL LET THE OPERATOR
C WATCH THE DIRECTION THE X VALUE IS
C GOING IN.
      3 PRINT 103,X
103 FORMAT(F14.8)
      4 IF(ABS(XOLD-X)-EPSI)1,1,2
      1 CONTINUE
      Y=EXP(Y)
      BETA=1./BETA
      XDT=X+.0
      PUNCH 102,DEG,FMON,X,Y
102 FORMAT(A3,1XA4,2X3HX =F10.5,2X2HKM4X7HDEFN X =E14.8,2X4HG/M3)
      PUNCH 113,HA,HPA,HPR
113 FORMAT(19HGEOPOT SCALE HT AT F9.4,1X4HKM =F9.5,11H, AT X KM =,
      1F10.7)
      PUNCH 109,BETA
109 FORMAT(35HGRADIENT OF GEOP SCALE HT ABOVE X =E14.8)
      PUNCH 114,FL,HBR,HR
114 FORMAT(23HGRADIENT OF MOL. TEMP. ,F4.1,10H FOR BTWN ,F5.0,4H TO ,F4.0)
      PUNCH 110,HB
110 FORMAT(38HGRADIENT OF MOL. TEMP. ZERO FOR H BTWN,F4.0,6H AND X)
      PUNCH 107
107 FORMAT(3X11HALTITUDE KM10X15HTEMP DEG KELVIN4X6HMOL WT2X,

```

```

112H DENSITY G/M34X11HSCALE HT KM)
PUNCH 108
108 FORMAT(11X6HGEOMET4X6HG FOPOT7X4HMOL.3X7HKINETIC28X6HGEOMET1X,
RHOX=Y
READ 104,DFG,R,GPHI
104 FORMAT(A3,F9.0,F8.5)
H=XPT
Z=R#H/(GPHI#R/9.80665-H)
C Z IS THE GEOMETRIC ALTITUDE
RHOH=PHA*(HPA/(HPA+BETA*(H-HA)))*((1.+BETA)/BETA)
C RHOH IS THE DENSITY
HH=(HPR+BETA*(H-X))*9.80665/GPHI*((R+7)/R)**2
C HH IS THE SCALE HEIGHT
TM=34.1632*(HPR+BETA*(H-X))
T=TM*(1.-2.375811E-03*(Z-90.))
C T IS THE TEMPERATURE
HPH=HPR+BETA*(H-X)
SM=28.9644-.0688133*(Z-90.)
C SM IS THE MOLECULAR WEIGHT
TM=TM+.005
T=T+.005
SM=SM+.005
HH=HH+.0005
HPH=HPH+.0005
C ROUND THE VALUES
PUNCH 105,Z,H,TM,T,SM,RHOH,HH,HPH
C PUNCH DATA CARD
105 FORMAT(F8.3,2XF8.3,3XF7.2,3XF7.2,3XF6.2,2XF12.5,2XF7.3,2XF7.3)
16HG FOPOT/)
C METHOD FOR FINDING NEXT EVEN KM.
XNEW=DRH(X)
XNEW=XNEW/2.
XNEW=DRH(XNEW)
XNEW=(XNEW*2.)+2.
XP=X*10.
XP=DRH(XP)/10.
IF(XNEW-XP-2.) 8,9,8
9 H=XP
GO TO 7
8 H=XNEW
7 IF(H-XPT)5,5,23
23 Z=R#H/(GPHI#R/9.80665-H)
RHOH=PHA*(HPA/(HPA+BETA*(H-HA)))*((1.+BETA)/BETA)
HH=(HPR+BETA*(H-X))*9.80665/GPHI*((R+Z)/R)**2
TM=34.1632*(HPR+BETA*(H-X))
T=TM*(1.-2.375811E-03*(Z-90.))
HPH=HPR+BETA*(H-X)
SM=28.9644-.0688133*(Z-90.)
FLM=34.1632*BETA
C FLM IS THE GRADIENT
TM=TM+.005
T=T+.005
SM=SM+.005
HH=HH+.0005

```

```

      HPH=HPH+.0005
      IF (Z-120.) 40,6,6
40  PUNCH 105,Z,H,TM,T,SM,RHOH,HH,HPH
      H=H+2.
      GO TO 7
      Z=R*X/(GPHI*R/9.80665-X)
      Z=DRH(Z)/2.
      Z=DRH(Z)*2.+2.
17  H=R*Z/(R+Z)*GPHI/9.80665
      RHOH=PHA*(HPA/(HPA+BETA*(H-HA)))*((1.+BETA)/BETA)
      SM=28.9644-.0688133*(Z-90.)
      HH=(HPR+BETA*(H-X))*9.80665/GPHI*((R+Z)/R)**2
      TM=34.1632*(HPR+BETA*(H-X))
      T=TM*(1.-2.375811E-03*(Z-90.))
      FLM=34.1632*BETA
      HPH=HPR+BETA*(H-X)
      TM=TM+.005
      T=T+.005
      SM=SM+.005
      HH=HH+.0005
      HPH=HPH+.0005
      PUNCH 105,Z,H,TM,T,SM,RHOH,HH,HPH
      IF (Z-120.) 10,11,11
10  Z=Z+2.
      GO TO 12
11  H=HR
      X=HR
      BETA=0.
12  Z=R*H/(GPHI*R/9.80665-H)
      HH=(HPR+BETA*(H-X))*9.80665/GPHI*((R+Z)/R)**2
      TM=34.1632*(HPR+BETA*(H-X))
      IF (Z-90.) 26,26,27
26  T=TM
      SM=28.96
      GO TO 28
27  T=TM*(1.-2.375811E-03*(Z-90.))
      SM=28.9644-.0688133*(Z-90.)
28  RHOH=HPR*EXP(-(H-HR)/HPR)
      HPH=HPR+BETA*(H-X)
      XPRIM=DRH(XPT)
      TM=TM+.005
      T=T+.005
      SM=SM+.005
      HH=HH+.0005
      HPH=HPH+.0005
      IF (H-XPRIM) 14,14,15
14  PUNCH 105,Z,H,TM,T,SM,RHOH,HH,HPH
      IF (H-HR) 16,41,16
41  IF (SENSE SWITCH 2) 16,17
C
C
17  H=H+1.
      GO TO 18
16  H=H+2.

```

SENSE SWITCH 2 ON, INCREASE THE HEIGHT BY 2.  
SENSE SWITCH 2 OFF, INCREASE THE HEIGHT BY 1.

```

      GO TO 18
15  Z=R*X/(GPHI*R/9.80665-X)
      Z=DRH(Z)/2.
      Z=DRH(Z)*2.+2.
21  H=R*Z/(R+Z)*GPHI/9.80665
      IF(H-HB)25,25,22
22  RHOH=PHB*FXP(-(H-HB)/HPB)
      HH=(HPB+BETA*(H-X))*9.80665/GPHI*((R+Z)/R)**2
      TM=34.1632*(HPB+BETA*(H-X))
      IF(Z-90.)29,29,30
29  T=TM
      SM=28.96
      GO TO 31
30  T=TM*(1.-2.375811E-03*(Z-90.))
      SM=28.9644-.0688133*(Z-90.)
31  HPH=HPR+BETA*(H-X)
      TM=TM+.005
      T=T+.005
      SM=SM+.005
      HH=HH+.0005
      HPH=HPH+.0005
      IF(H-XPT)19,20,20
19  PUNCH 105,Z,H,TM,T,SM,RHOH,HH,HPH
25  Z=7+Z.
      GO TO 21
20  PUNCH 111,FLM,HA
111 FORMAT(23HGRADIENT OF MOL. TEMP. F10.5,2X19HDEG/KM FOR H BTWN X,
14H AND,F9.4//)
      GO TO 13
      END

```

## PROGRAM 2

The program for defining a two-layer model by the evaluation of an algebraic function, which replaces the successive approximation method.

# PROGRAM 2

```

C      SOURCE DECK FOR TWO-LAYER TRANSITION MODEL ATMOSPHERE
C      BETWEEN UPPER-LEVEL AND LOWER-LEVEL BOUNDARY CONDITIONS
C      WHEN THE FOLLOWING CONDITIONS REGARDING TEMPERATURE-ALTITUDE
C      GRADIENT PREVAILS
C      1. IT HAS A DIFFERENT CONSTANT VALUE FOR EACH LAYER.
C      2. IT HAS A POSITIVE VALUE FOR THE UPPERMOST LAYER,
C      3. IT HAS A ZERO VALUE FOR THE LOWER LAYER.
100  FORMAT(F10.1,2XE12.6,1XF10.3,2XF10.1,2XE12.6,1XF10.3)
51  READ 100,HN,RHON,TN,H0,RH00,T0
      BEGIN TRACE
      Q=3.4163195E-02
      HX0=(LOGF(RHON/RH00)+HN*Q/TN-(1.+H0*Q/(T0-TN))*LOGF(T0/TN))
      HX0=HX0/(Q/TN-(Q/(T0-TN))*LOGF(T0/TN))
      GLX0=(T0-TN)/(H0-HX0)
      RHOX0=RHON*EXPF(-Q*(HX0-HN)/TN)
120  FORMAT(21X33HDEFINITION OF THE TWO-LAYER MODEL)
111  FORMAT(1H )
112  FORMAT(10X5HLEVEL,5X1HH,11X3HRHO,11X1HT,11X1HL)
113  FORMAT(18X43HMETERS          KG/M3          DEG K          DEG/M)
114  FORMAT(10X13,2XF10.1,2XE12.6,1XF10.3,2XE12.6)
115  FORMAT(10X13,2XF10.1,2XE12.6,1XF10.3,3X11H.000000E+00)
      PUNCH 111
      PUNCH 111
      PUNCH 120
      PUNCH 111
      PUNCH 112
      PUNCH 113
      PUNCH 111
      LEVEL=0
      PUNCH 114,LEVEL,H0,RH00,T0
      LEVEL=LEVEL+1
      PUNCH 114,LEVEL,HX0,RHOX0,TN,GLX0
      LEVEL=LEVEL+1
      PUNCH 115,LEVEL,HN,RHON,TN
      END TRACE
      END

```